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# Booster RF Cavity Replacement

Thomas Kroc

PIP-II Collaboration Meeting

9-10 November 2015

# Why?

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- While the existing cavities have been refurbished, they are still 40 years old.
- PIP II operations will leave no extra operating margin.
- Uncertain operational impact of needing to run all cavities at maximum performance 24/7.

# PIP & PIP-II high level performance goals

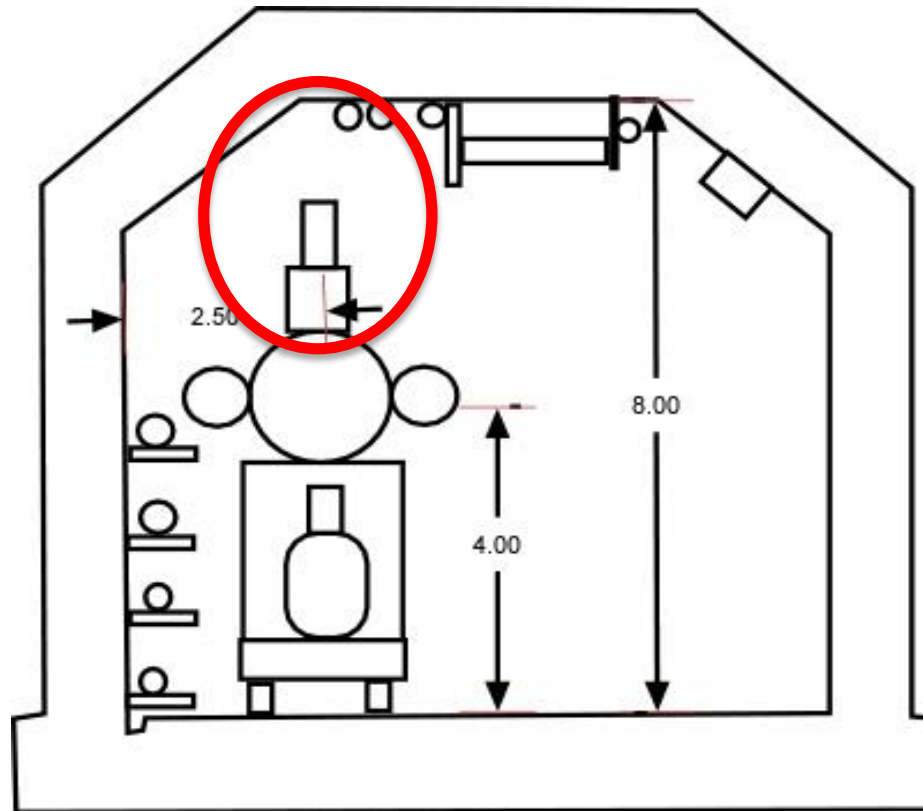
Beam Performance Parameter	PIP	PIP-II	
Injection Energy	400	800	MeV
Linac Particle Type	H <sup>-</sup>	H <sup>-</sup>	
Linac Beam Current	27	2	mA
Linac Beam Pulse Length	0.03	0.5	msec
Beam Capture	Adiabatic Paraphase	Bucket to Bucket	
Booster Pulse Repetition Rate	15	20	Hz
Booster Protons per Pulse	$4.2 \times 10^{12}$	$6.4 \times 10^{12}$	
Booster Beam Power @ 8 GeV	80	160	kW
Beam Emittance (6s, normalized; ex=ey)	<18	<18	$\pi$ mm-mrad
Delivered Momentum Spread (97% full height)	12.2 Momentum Spread (97% full	12.2 Momentum Spread (97% full	MeV Momentum Spread (97% full
Delivered Longitudinal Emittance (97%)	.08	.08	eV-sec

# PIP & PIP-II RF Parameters

Cavity Performance Parameter	PIP	PIP-II	
Frequency Sweep	37 to 53	44.7 to 53	MHz
Cavity Tuning (Bias Supply Max Current)	3000	3000	amps
Modulator Voltage (Max: Anode – drop)	30	30	kV
Higher Order Mode	< 1000	<1000	Ohms
Aperture	~ 3	~3	inch
*Total Voltage	1000	1100	kV
Overhead Voltage	100	100	kV
Duty Cycle	50	50	%
Cavity Q	300 to 1250		
Shunt Impedance	17 to 61.25		k Ohms
LCW Cooling Temp (actual)	95 (88 – 94)	95 (88 - 94)	F
LCW Flow	100	100	PSI
Forced Air Cooling	Yes	Yes	

\* Sum of gap voltages at peak power, overhead allows for running with reduced # of cavities.

# Tunnel Constraints



Must fit in existing tunnel, limitation of options for new Pas.

# Cavity Voltage

- Present
  - 830 kV – 950 kV, present operating range depending upon beam requirements and cavity repair status.
  - < 850 kV, losses increase for  $4.2E12$ /pulse.
    - requires a minimum of 17 cavities at the nominal voltage 50 kV or 25 kV/gap.
- PIP II requirement
  - 1.2 MV ( 1.1 MV total + 0.1 MV overhead )

	Voltage per Cavity			
# of cavities	Present 870 kV	Soon 950 kV	Next Year 1005 kV*	Replacement 1200 kV
19	45.8 kV			
20		47.5 kV		60 kV
21			47.8 kV	57 kV
22			45.7 kV	55 kV

\* If funding allows

- Plan to run similar to MI, all cavities on, voltage fixed/regulated as needed.

# Cavity Tuning and Drive System

- Will use existing hardware which was all recently upgraded for PIP
  - New solid state driver system
  - Upgraded bias supplies
  - New anodes – higher power
  - Additional cooling (air & LCW) systems for RF systems
  - Upgrades on low level controls
- This task of the PIP project is replacement of cavities only

# Other cavity performance factors

- **Beam Loading and Power Requirements**

- Each cavity must meet the specified voltage while accelerating up to 1000ma of beam (at a synchronous phase of ~40 degrees (synchrotron definition, 90 degrees at crest)) with 2-3 of the 84 buckets empty.
- The loaded cavity shall be designed to operate with up to 150 kW RF power from a CPI (EIMAC) Y-567B tetrode power tube. Although rated to operate at higher power up to 200 kW, for lifetime considerations operating at a lower power is preferable.

- **Cavity Impedance and Spurious Modes**

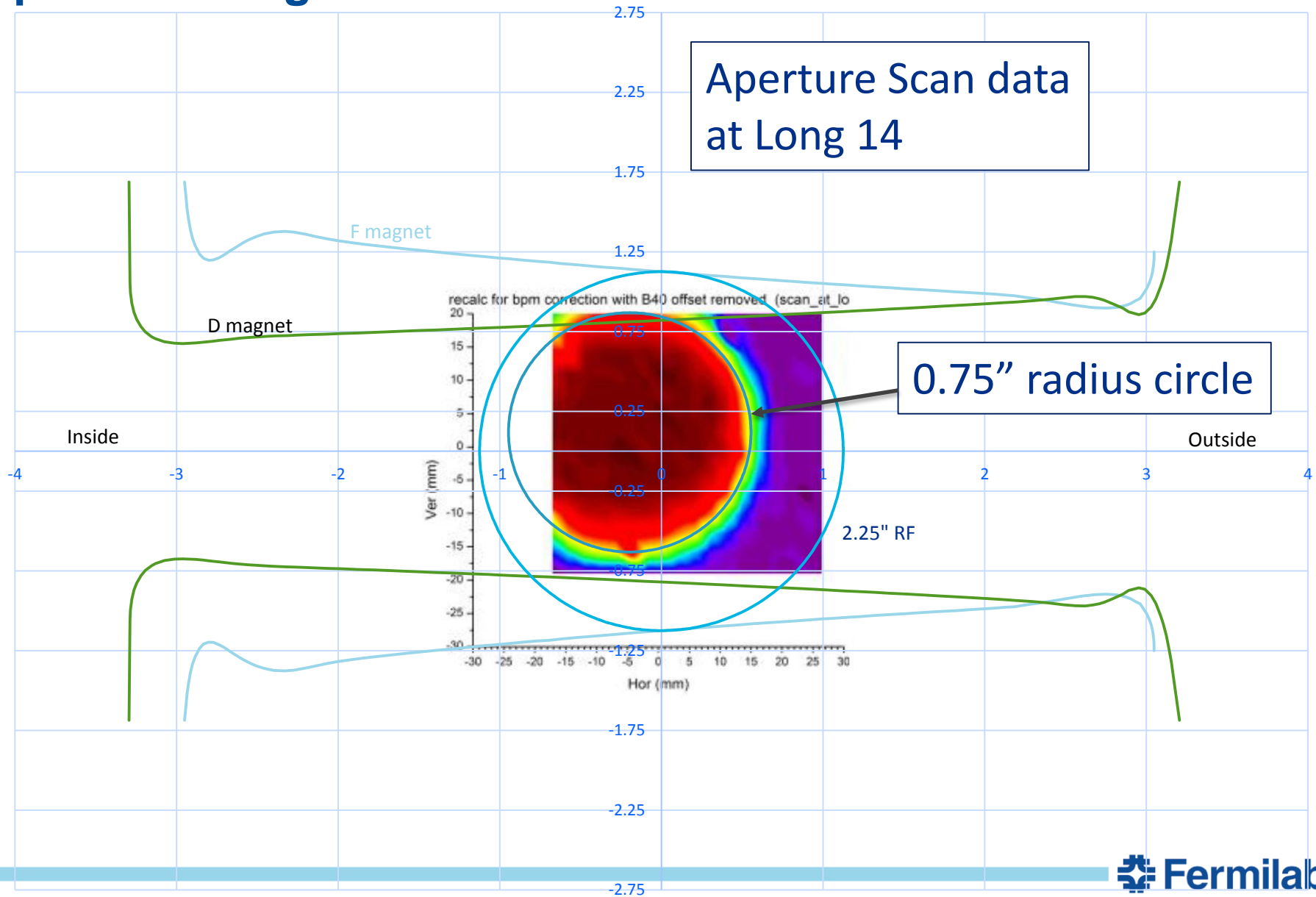
- The cavity shall be designed for  $R/Q = 50$  ohms and the impedance of all higher order and spurious modes shall be  $\leq 1000$  ohms.

- **Multipacting**

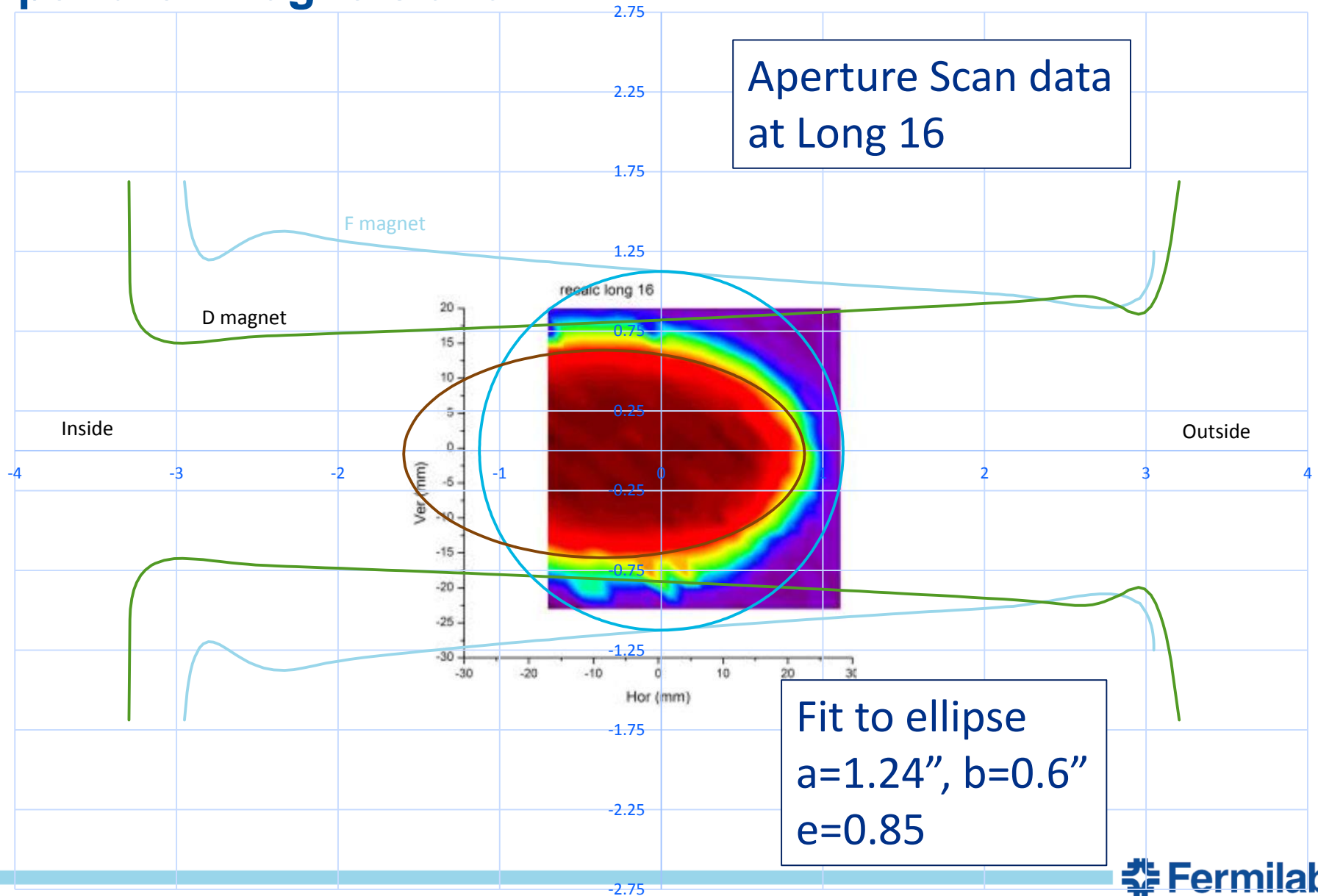
- The cavity must be able to turn on and run at any voltage between 25% and 100% of the specified operating voltage over the full frequency range without operationally significant multipacting at the nominal operating vacuum pressure.



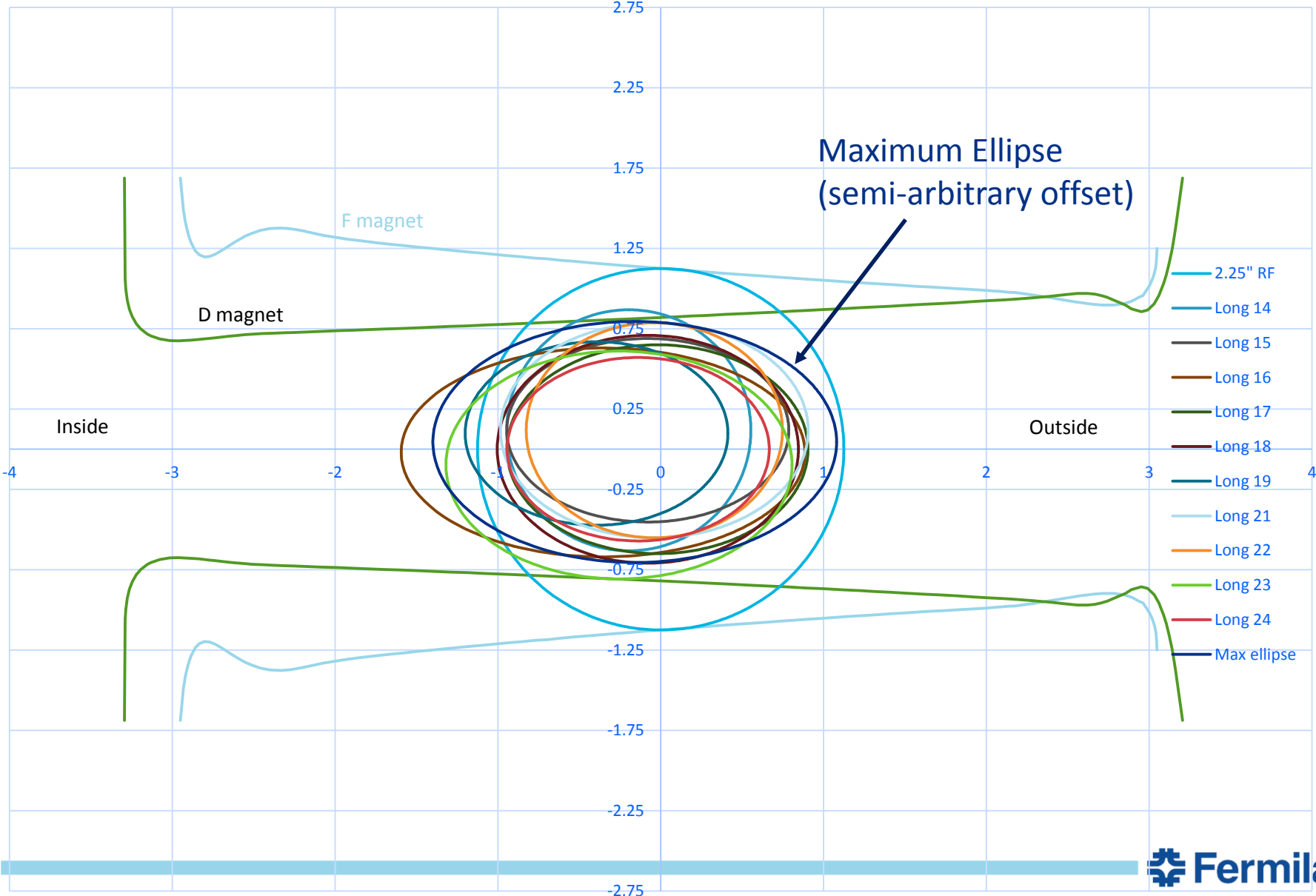
# Aperture - Magnets and RF



# Aperture - Magnets and RF



# Aperture - Ellipse using maximum parameters



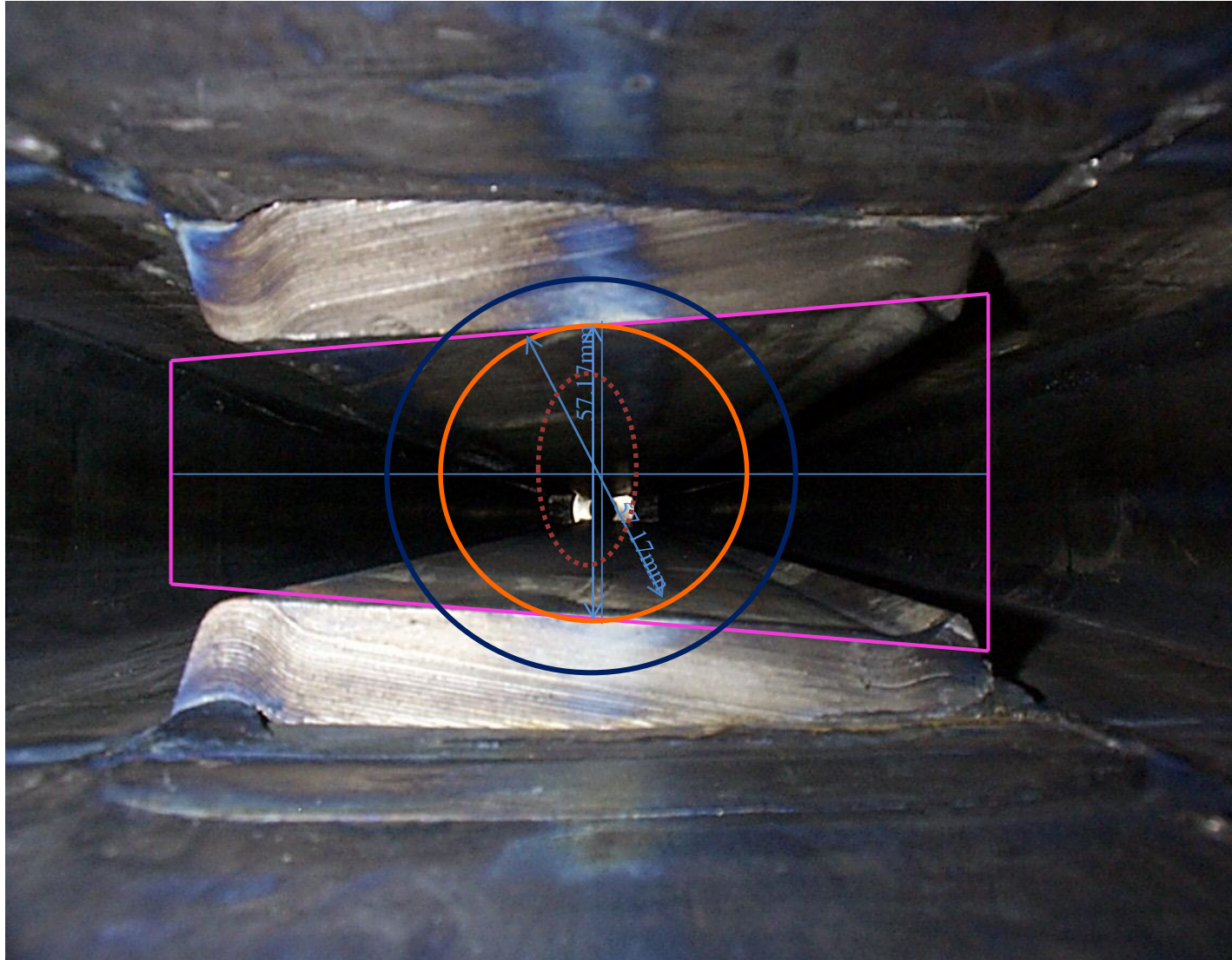
# Aperture - Conclusion

	a (inch)	b (inch)	area (in <sup>2</sup> )
average	0.9113	0.6519	1.87
max	1.24	0.75	2.92
Ratio (max/ave)	1.36	1.15	1.57
New aperture radius	1.53	1.29	6.22

↓  
Radius = 1.4

3" beam pipe will provide 0.1" to 0.2" margin

# Aperture – Second Look



- Vertical aperture limited by magnets
- Horizontal aperture limited by cavities

# PIP-III Beam Parameters

Table 3	Booster (PIP)	PIP II	New RCS (PIP III)
<b>Pulse Intensity</b>	4.3E12	6.5E12	30E12
<b>Peak RF Beam Current</b>	.86 amps	1.3 amps	6 amps
<b>Cycle Rep Rate</b>	15	20	20
<b>Injection energy</b>	.4 GeV	.8 GeV	2 GeV*
<b>Extraction energy</b>	8 GeV	8 GeV	8 GeV
<b>Revolution time</b>	2.22 to 1.59 us	1.88 to 1.59 us	1.66 to 1.59 us

\*Representative value (still under discussion)

# PIP-III Cavity Parameters

Table 4	Booster (PIP)	PIP II	New RCS (PIP III)*
<b>Frequency Sweep</b>	37 to 53 MHz	44 to 53 MHz	50 to 53 MHz
<b>Peak DP/DT MeV/.1ms</b>	376	470	387
<b>Peak eV/turn</b>	606	755	620
<b>Harmonic #</b>	84	84	84

\* No design available – basic assumptions about beam current and injection energy

# Review

- Consensus
  - New cavities – yes
  - Larger bore necessary for PIP-III suggested but impact on design not understood
  - Continue simulation efforts for  $\parallel$  &  $\perp$  bias cavities
  - Prototypes for  $\parallel$  &  $\perp$  bias cavities
- Questions
  - Wait for results of  $\perp$  bias ?
  - Cost trade-off between copper and garnet
- Additionally
  - Instrumentation, feedback, and control needs to be upgraded for reliable operation at projected beam powers



# Conclusion

- No upstairs systems are involved
  - All necessary upgrades will have been completed as part of PIP
- Physical constraints remain the same – no tunnel modifications anticipated
- Beam parameters for PIP-II are set
- Cavity specs are complete and can be applied to either:
  - Parallel bias cavity or
  - Perpendicular bias cavity
- Major cavity specs are compatible with PIP-III/RCS
  - Detailed specs will determine whether cavities can be used
- Work ramping up in FY16 with plans to test prototype in FY17



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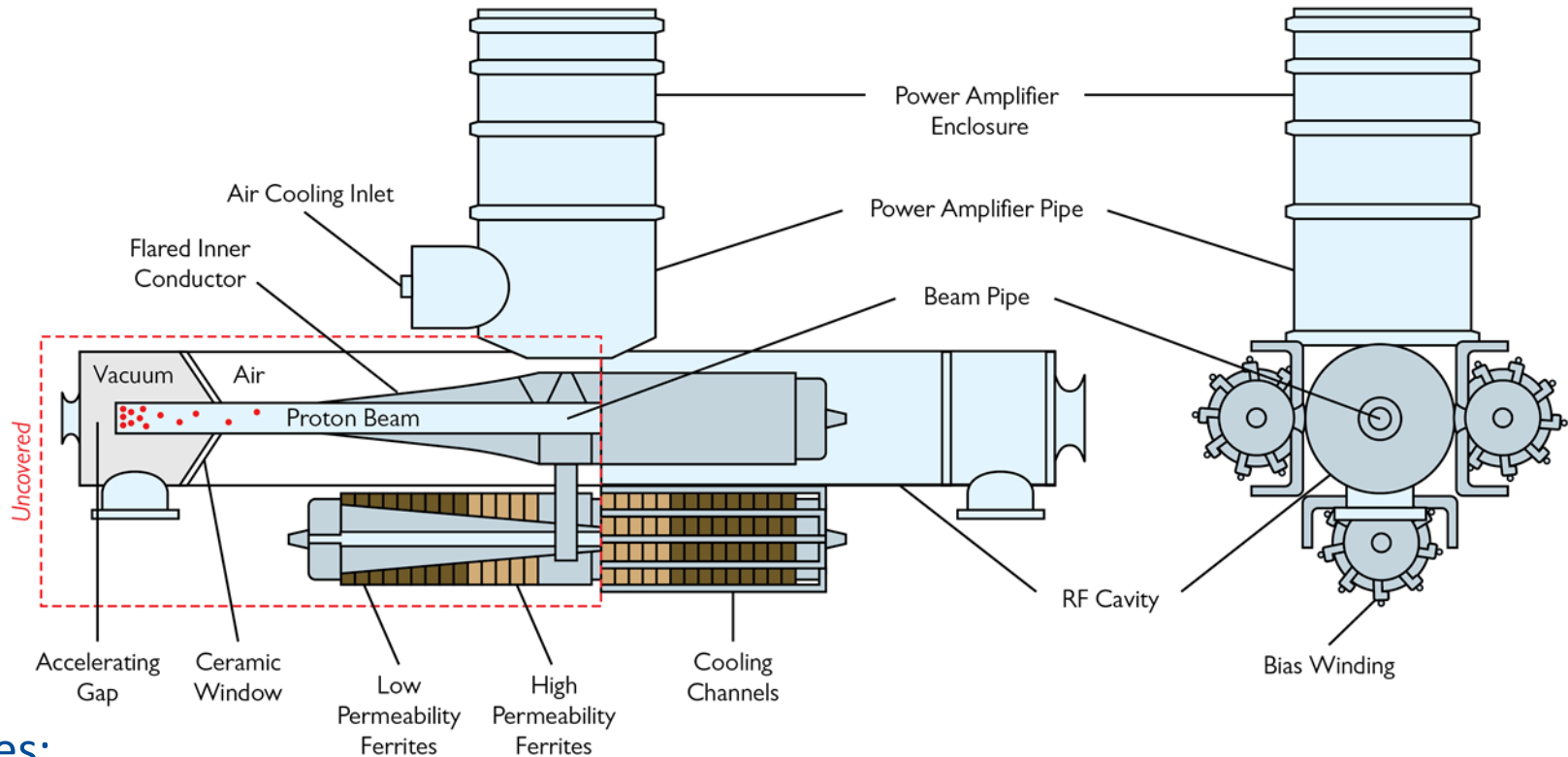
# **Electromagnetic Modeling of Fermilab's Booster Cavity**

Mohamed Hassan

Workshop on Booster Performance and Enhancements

24<sup>th</sup> Nov 2015

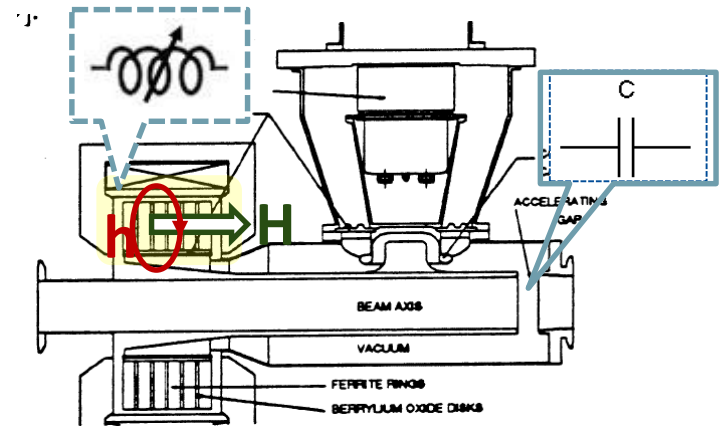
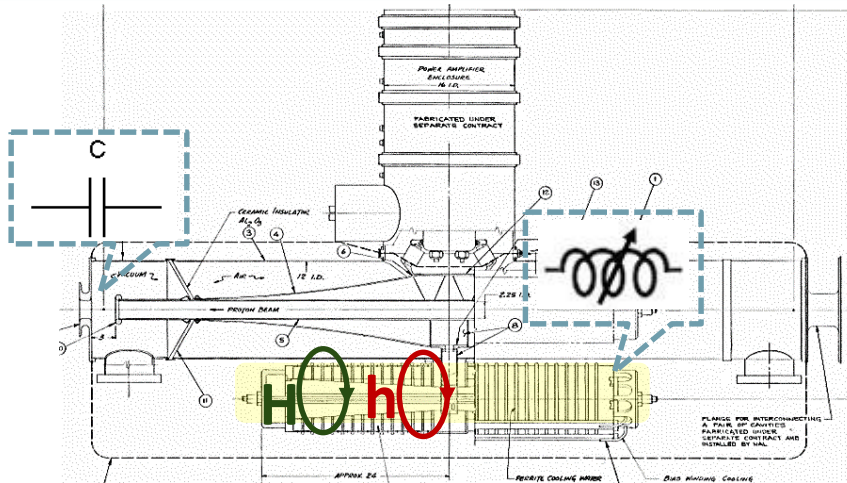
# Geometry of Fermilab's Booster Cavity



## Issues:

- RF heating with increased duty cycle (resolved for 15 Hz by additional air/water cooling)
- Activation of beam pipe (need for larger bore)
- Occasional voltage breakdown (need for better tuner connection)

# Tunable Booster Cavities



## Parallel Biased

Bias Field is Parallel to the RF Field

$$H\hat{\phi} + h\hat{\phi} = (H + h)\hat{\phi}$$

Ferrites with High Saturation Magnetization (Ni-Zn)

Larger values of  $\mu$  (Larger Losses, Lower Q)

## Perpendicular Biased

Bias Field is Perpendicular to the RF Field

$H\hat{z} + h\hat{\phi} = \text{rotating (on cone) magnetic vector - Gyromagnetic Resonance } H=f/2.8$

Ferrites with Relatively Low Saturation Magnetization (Mn-Zn)

Smaller values of  $\mu$  (Smaller Losses, Larger Q)

# Comparison Between Existing Relevant Booster Cavities

	FNAL Booster	TRIUMF	SSCL LEB	EHF-Booster
Energy Range [GeV]	0.4-8.0	0.45-3.0	0.6-11	1.2-9.0
Bias	Parallel	Perpendicular	Perpendicular	
Frequency [MHz]	37.7-53.3	46.1-60.8	47.5-59.8	50.5-56.0
Peak Gap Voltage [kV]	2*27	62.5	127.5	2*36
Cavity Length [m]	~2.4	~1.23	~1.25	~3.25
Accelerating Time [ms]	35	10	50	20
Repetition Rate	7	50	10	25
Ferrite Material	Ni-Zn	Yttrium Garnet	Yttrium Garnet	
Ferrite Material	Toshiba, Stackpole	TT-G810	TT-G810	
Cavity Q	250-1200	2200-3600	2800-3420	
Cavity R/Q	50	35	36	
Status	Operating	Prototype	Prototype	

Development of perpendicular-biased cavities didn't pass prototype stage

# Why Perpendicular Biased Cavity Could Achieve Higher Voltage Gradient?

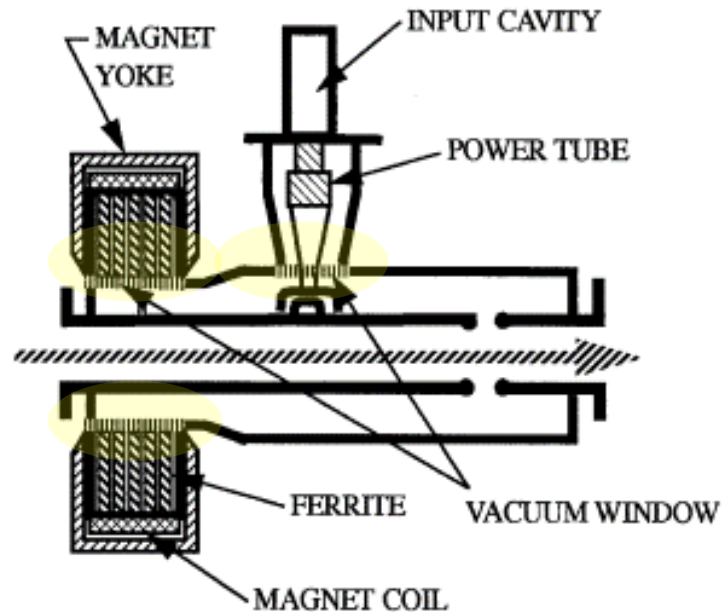
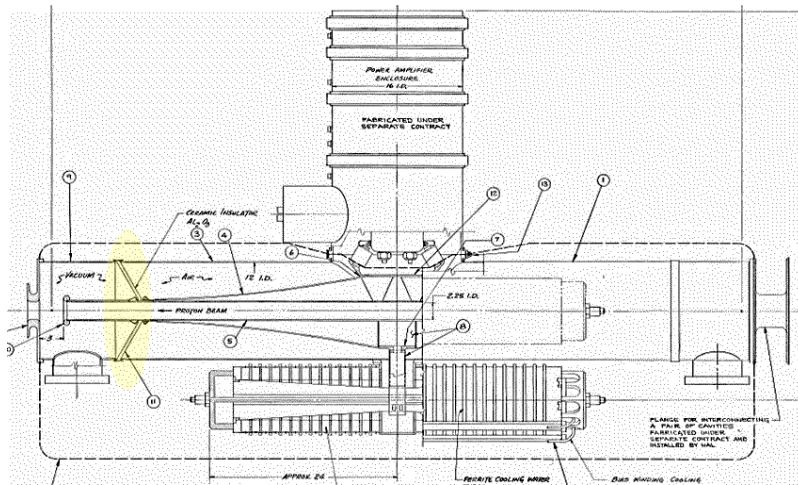
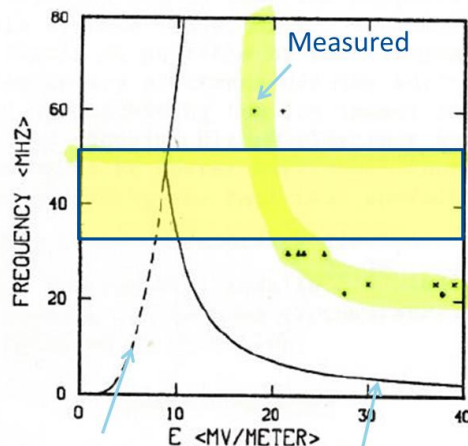


Figure 1. LEB prototype cavity.

- Air fills most of the cavity volume (breakdown  $\sim 30$  kV/cm)
- Vacuum windows are nearby the gap
- Tuner is filled with air



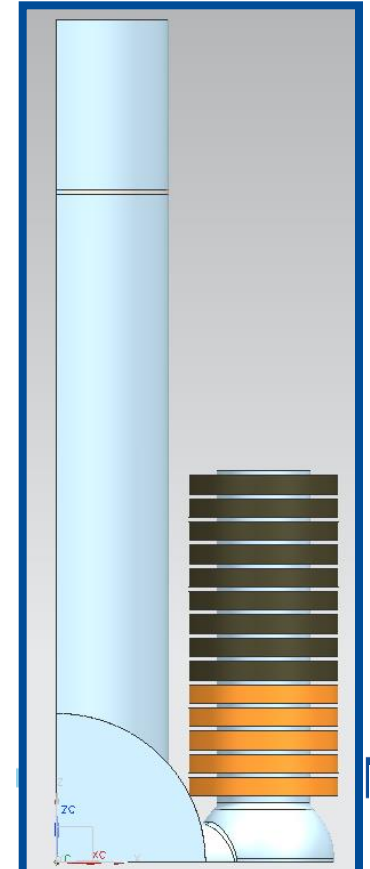
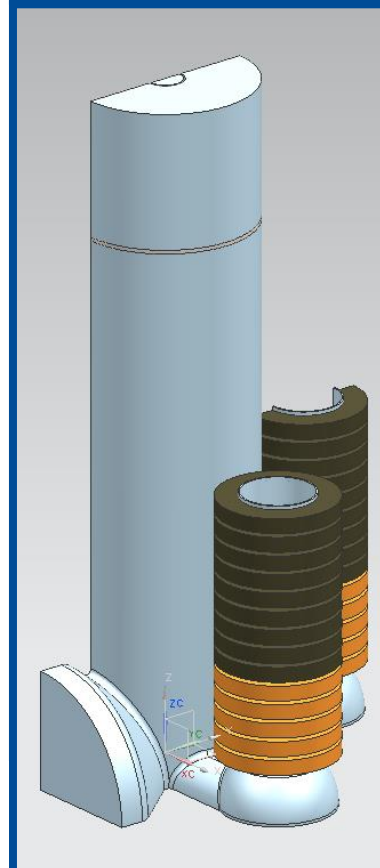
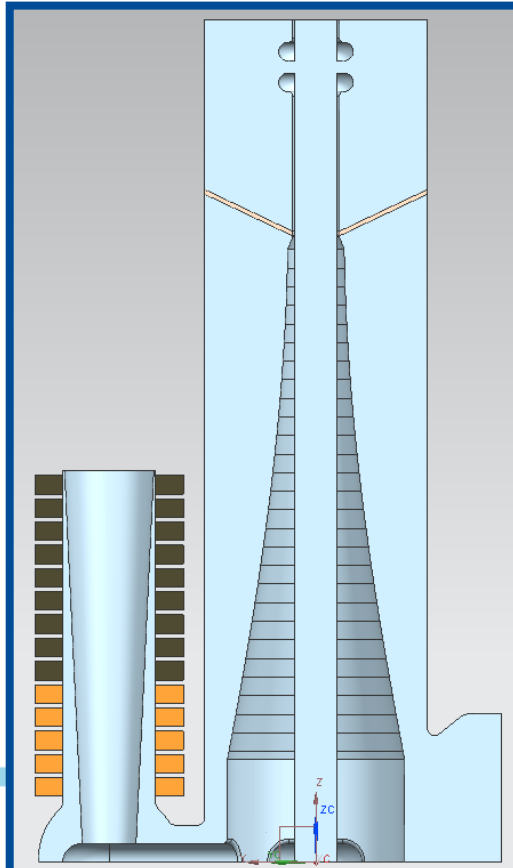
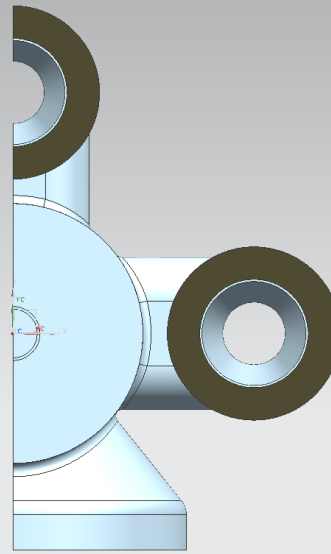
In Air  $\sim 3$  MV/m (30 kV/cm)

In Vacuum (according to Kilpatrick) is  $\sim 10$  MV/m  
(theoretical) 18 MV/m (measured)

- Vacuum fills most of the cavity volume (breakdown  $\sim 100$  kV/cm)
- Vacuum windows are right away on the tuner connection
- Tuner is filled with dielectric

# Full 3D Model

- Realistic Tuner with all the fine details
  - 5 Toshiba Ferrites
  - 9 Stackpole Ferrites
  - Flared Inner Conductor
- Realistic Tuner Connection



## Possible Changes to the Current Design

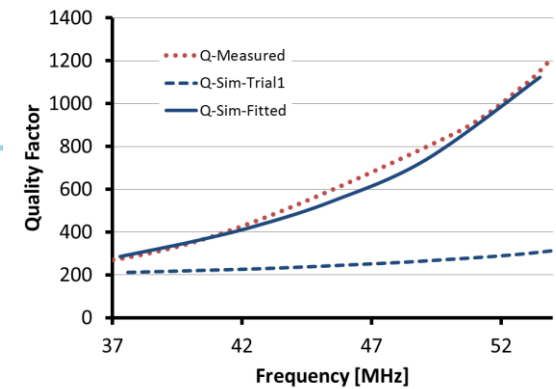
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- Rounding the stem corners with large radius  $>0.25''$  to reduce the risk of voltage breakdown in air-filled regions
- Enlarging the stem connection between the tuner and the cavity would help to reduce tuner losses
- Improve the connection of the vacuum window and cavity to reduce ceramic window failures
- Can we fill the tuner with another medium other than air?



# Regular Cycle 7.5Hz vs 15Hz

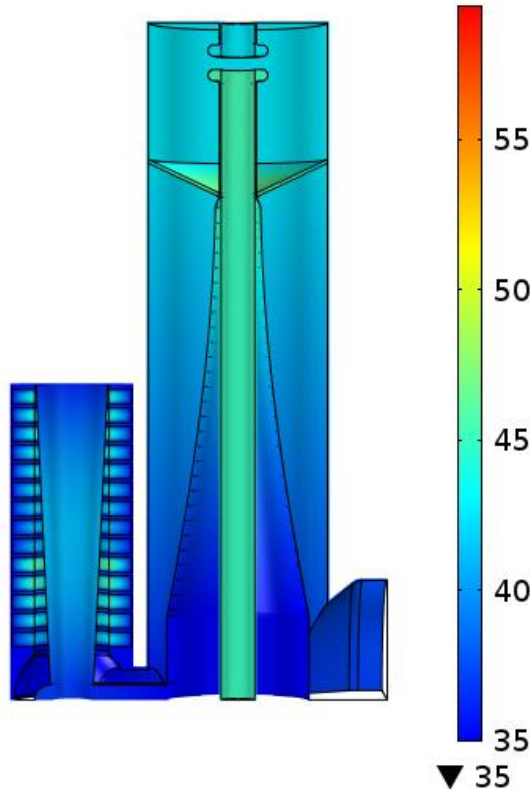
- Simulated Q has been fitted to the measured one by adjusting the magnetic loss tangent with frequency



55 kV, 7.5 Hz ▲ 47.2

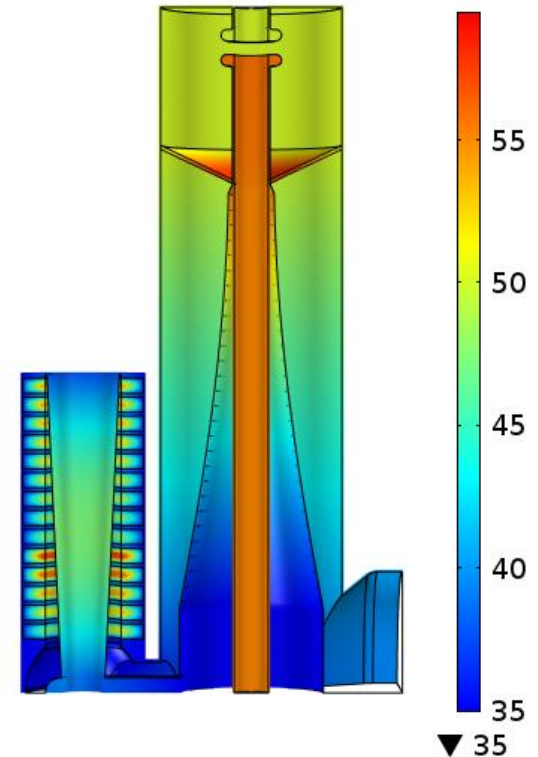
Max T=47.2° C

Constant Temp  
Boundaries



55 kV, 15 Hz ▲ 59.4

Constant Temp  
Boundaries



# CW Simulation vs Measurements Results

Measurements data were collected for various CW fixed frequency cases (22kV)

Simulations	50 MHz	45 MHz	40 MHz
<b>Frequency [MHz]</b>	<b>49.998</b>	<b>45.0163</b>	<b>39.979</b>
<b>Unloaded Quality Factor</b>	<b>773</b>	<b>513</b>	<b>348</b>
Gap Volatge [kV]	22.00	22.00	22.00
Volume Losses [kW]	5.01	9.25	16.88
Surface Losses [kW]	1.03	1.09	1.18
<b>Total RF Losses [kW]</b>	<b>6.04</b>	<b>10.34</b>	<b>18.07</b>

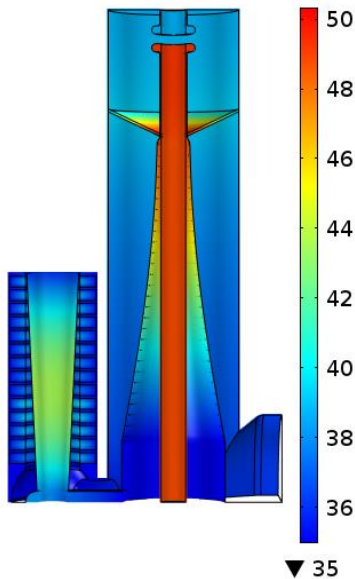
	50 MHz	45 MHz	40 MHz
Total RF Losses [kW]	6.04	10.34	18.07
P_RF_Water [kW]	5.48	8.58	13.79
<b>Descrepancy %</b>	<b>10.34</b>	<b>20.56</b>	<b>31.02</b>

Measurements	50 MHz	45 MHz	40 MHz
Bias Current [A]	1290	640	325
Bias Voltage [V]	5.296	2.544	1.286
Pbias [kW]	6.83	1.63	0.42
Anode Volatge [kV]	10	10	10
Plate Current [A]	2.2	2.4	3.06
Input RF Power [kW]	22	24	30.6
<b>Frequency [MHz]</b>	<b>49.898</b>	<b>44.878</b>	<b>40.056</b>
<b>Unloaded Quality Factor</b>	<b>678</b>	<b>435</b>	<b>330</b>
Gap Volatge [kV]	22	22	22
f_water [Hz]	200.2	200	197.7
K-Factor	938	938	938
Water Flow [gpm]	12.81	12.79	12.65
dT_bias	1.95	0.45	0.12
P_bias [kW]	6.59	1.52	0.40
dT_withAir	3.28	2.70	4.19
dT_noAir	3.57	2.99	4.25
P_air [kW]	0.98	0.98	0.20
P_Water [kW]	12.07	10.10	14.19
<b>P_RF [kW]</b>	<b>5.48</b>	<b>8.58</b>	<b>13.79</b>

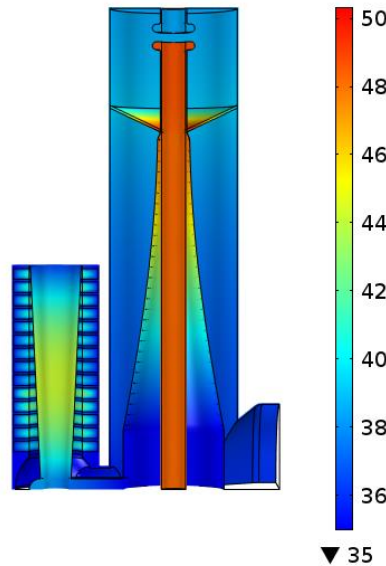
Measurement data provided by **John Reid**

# Simulation vs Measurements

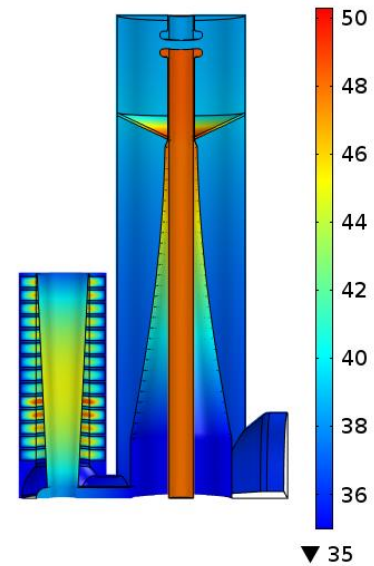
50 MHz, 22 kV, CW



45 MHz, 22 kV, CW



40 MHz, 22 kV, CW

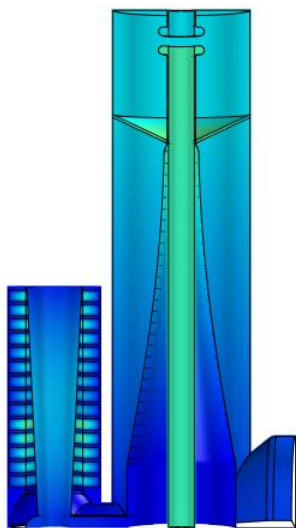


50 MHz	Tfront [C] (FR99T)	Tback [C] (BA99T)	Tcavity [C] (BA99RT)	Tbottom [C] (AD99DT)
Base	34.02	33.49	32.49	32.72
Air is ON Steady State	40.55	38.07	36.52	36.74
Air is OFF Steady State	<b>49.18</b>	<b>46.11</b>	<b>47.44</b>	<b>41.01</b>
45 MHz	Tfront [C] (FR99T)	Tback [C] (BA99T)	Tcavity [C] (BA99RT)	Tbottom [C] (AD99DT)
Base	32.47	31.97	30.31	32.15
Air is ON Steady State	38.44	36.33	34.88	35.41
Air is OFF Steady State	<b>45.96</b>	<b>43.32</b>	<b>44.57</b>	<b>39.25</b>
40 MHz	Tfront [C] (FR99T)	Tback [C] (BA99T)	Tcavity [C] (BA99RT)	Tbottom [C] (AD99DT)
Base	31.66	31.15	29.61	31.27
Air is ON Steady State	38.00	36.00	34.00	35.00
Air is OFF Steady State	<b>43.57</b>	<b>41.36</b>	<b>42.3</b>	<b>38.28</b>

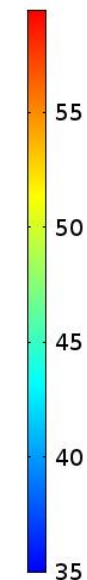
	Parallel Biased		**Perpendicular Biased	
Length [m]	2.3		1.1	
Height [m]	0.56		0.5	
Aperture [in]	2.25		3.25	
Volume of Ferrites [m <sup>3</sup> ]	0.04216		0.03626	
Cost				
Gap Voltage [kV]	55		55	
Frequency Sweep [MHz]	37.3	53.8	37.2	53.8
Permittivity	12.0*(1-j*0.005) 10.5*(1-j*0.005)		14.0*(1-j*0.00015)	
Permeability	8.40*(1-j*0.0051) 5.25*(1-j*0.0037)	3.00*(1-j0.0018) 1.88*(1-j*0.0013)	4*(1-j*0.003)	1.5*(1-j*0.00036)
Q	285	1102	385	4004
Energy [mJ] CW	171.59	59.40	95.79	68.35
Volume Losses CW	141.27	18.23	57.96	5.58
Surface Losses CW	6.98	5.92	0.36	0.72
Total Losses CW	148.25	24.15	17.1	3.0
E <sub>max</sub> in Air [MV/m]	1.67	0.91	-	-
E <sub>max</sub> in Vacuum [MV/m]	2.2	2.2	4.6	4.6
E <sub>max</sub> in Ferrite [MV/m]	0.21	0.10	0.32	0.21
T <sub>max</sub> [C] at 7Hz/15Hz	47.2/59.4		77.2/119.0	
Energy [mJ] at 7Hz/15Hz	0.25/0.5*66.86		0.25/0.5*47.51	
Total Power Loss [kW] at 7Hz/15Hz	14.4/28.9		7.23/14.5	

55 kV, 7.5 Hz

Constant Tem  
Boundaries

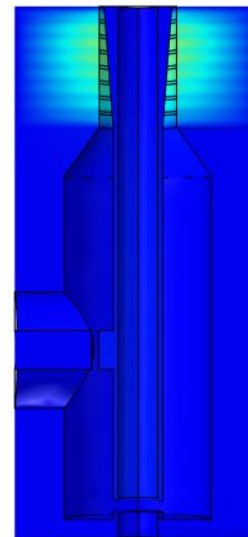


▲ 47.2

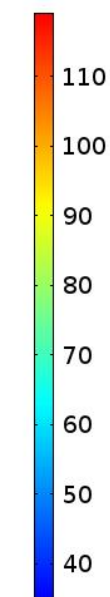


55 kV, 7.5 Hz

Constant Temp  
Boundaries

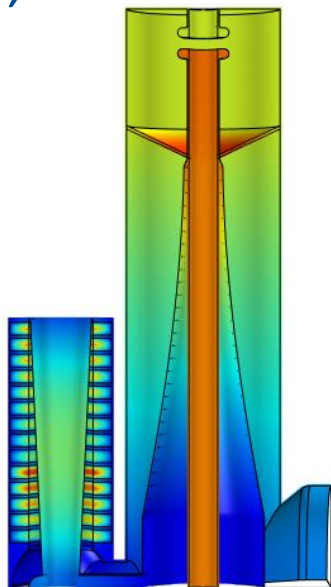


▲ 77.2

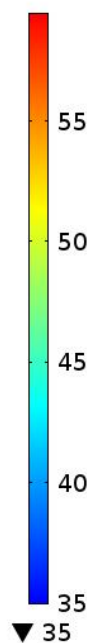


55 kV, 15 Hz

Constant Ten  
Boundaries

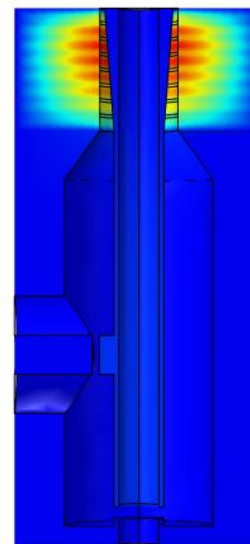


▲ 59.4

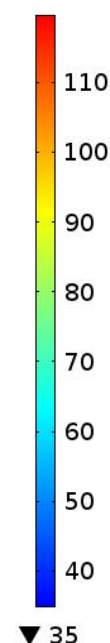


55 kV, 15 Hz

Constant Temp  
Boundaries



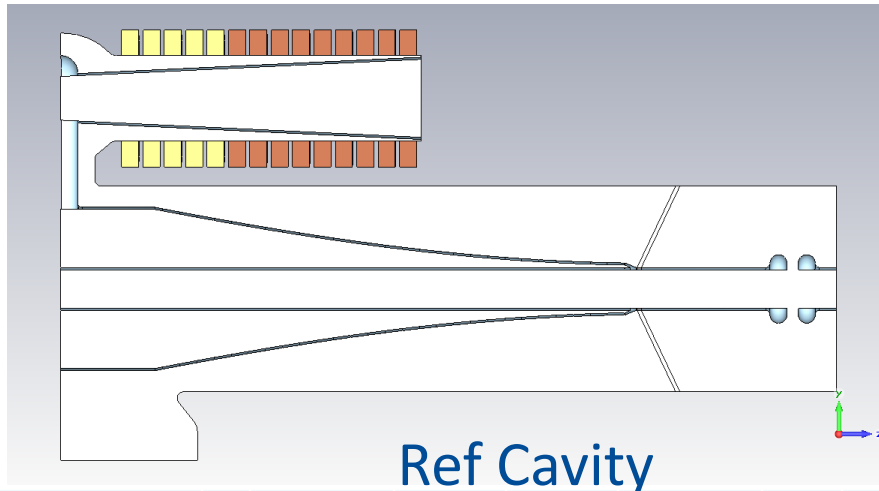
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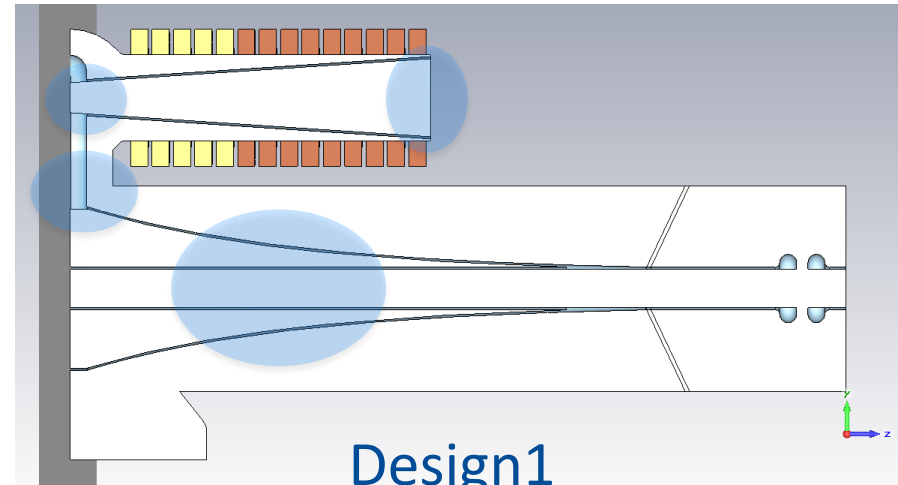
\*Cavity geometry is based on TRIUMF with no further optimization

# Preliminary New Design

- Carried out full parametric study
- Identified changes that can help lower the losses in the cavity



Ref Cavity

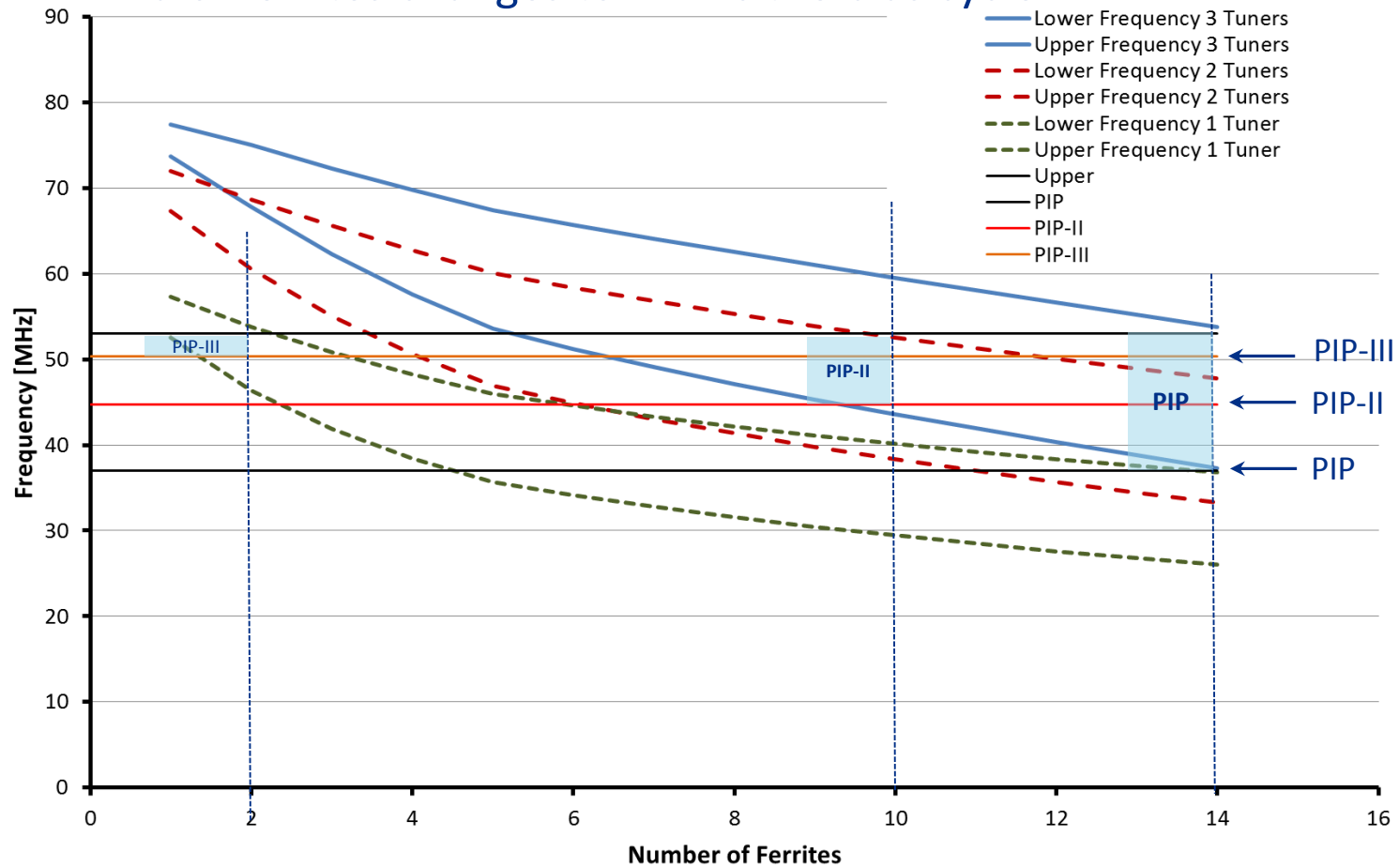


Design1

		mu=8.4 mu=3				Energy needed for 55 kV											
		fa1 [MHz]	f1 [MHz]	f2 [MHz]	fa2 [MHz]	Qa1	Q1	Q2	Qa2	Ea1[mJ]	E1 [mJ]	E2 [mJ]	Ea2[mJ]	Eav [mJ]	Eint [mJ]	BW[MHz]	
Ref Cavity		37.3	37.3	53.5	53.5	286	286	1123	1123	42.9	42.9	14.8	14.8	28.85	19.9065	16.2	
		mu=11	mu=8.4	mu=3	mu=3.5												
Design1: Rconn=2.5, Rtunner1=1, Ls=1, Rpipe=1.125, C=- 0.08		37.5	41.5	55.3	53.6	229	322	1616	1230	28.6	21.3	8.4	9.4	19	13.11	13.8	

- Sacrifice for 2.4 MHz in bandwidth that will need to be compensated for by biasing less the ferrites
- About 30% saving in power loss

# Mu of ferrites changes to mimic the bias cycle



	PIP [37-53 MHz]	PIP-II [44.7-53 MHz]	PIP-III [50.3-53 MHz]
3-Tuner Design [37-53 MHz]	✓	✓	✓
2-Tuner 10F/H [43.6- 53 MHz]		✓	✓
1-Tuner 2F/H [46.4-53.7 MHz]			✓

# Conclusion

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- A full detailed 3D model to the current cavity has been built
- Current cavity has been subject to extensive electromagnetic and thermal analysis
- We were able to compare simulation and measurements for CW operations with fairly good agreement
- Further measurements are planned
- We carried out a full parametric study to the current cavity geometry
- Modifications to the current cavity have been proposed
- We have also explored the possibility of operating the cavity under PIP-II and PIP-III frequency sweep scenarios

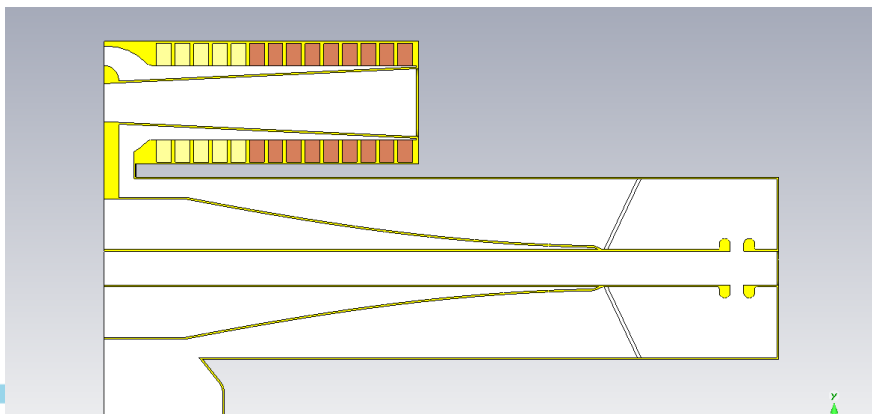


# Fermilab's Booster Cavity

## Criteria of Comparison?

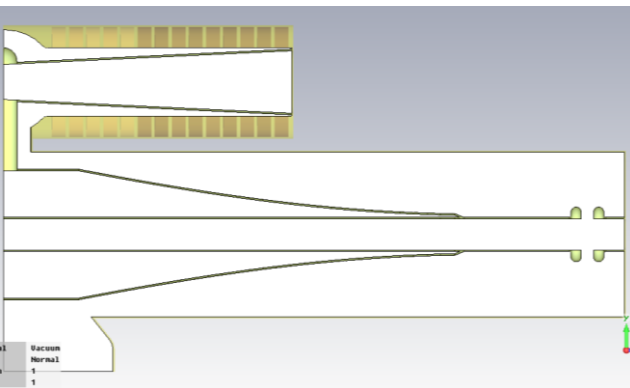
- With eigen-mode simulation, the quality factor and energy (not the power) that would produce a required gap voltage could be calculated
- Decreasing the energy needed for 55 kV gap voltage (increasing the Q) simply means less power loss inside the cavity thus less heating
- These performance indicators will be calculated at two permeability values, namely; 8.4 and 3.0 that corresponds to the edge frequencies of the current booster operation

		$\mu=8.4$	$\mu=3$	Q1	Q2	Energy needed for 55 kV					BW[ MHz]
		f1 [MHz]	f2 [MHz]			E1 [mJ]	E2 [mJ]	Eav [mJ]	Eint [mJ]		
Ref Cavity		37.3	53.5	286	1123	42.9	14.8	28.85	19.9065		16.2

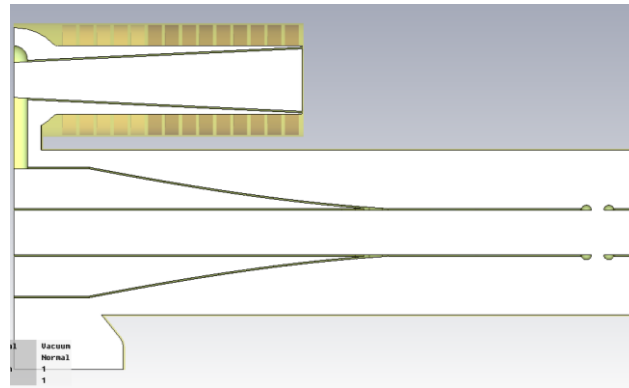


Simple ~Integral  
Average Average

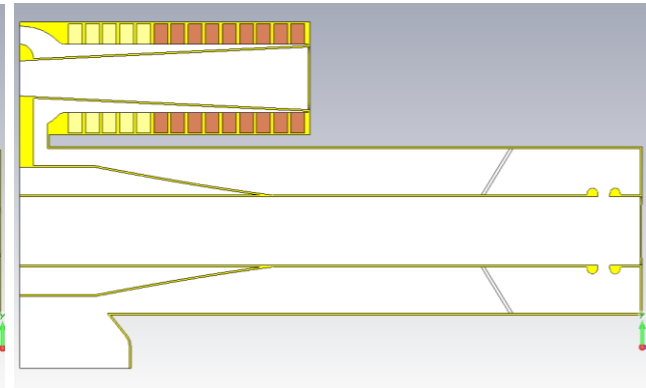
# Bore Radius Effect on the Cavity Performance



$R_{\text{pipe}}=1.125$



$R_{\text{pipe}}=1.625$



$R_{\text{pipe}}=2.5$

$R_{\text{pipe}}$		$\mu=8.4$	$\mu=3$	Energy needed for 55 kV						BW[ MHz]
		f1 [MHz]	f2 [MHz]	Q1	Q2	E1 [mJ]	E2 [mJ]	Eav [mJ]	Eint [mJ]	
1		37.4	53.9	285	1100	43.6	15.2	29.4	20.286	16.5
<b>1.125</b>		<b>37.3</b>	<b>53.5</b>	<b>286</b>	<b>1123</b>	<b>42.9</b>	<b>14.8</b>	<b>28.85</b>	<b>19.9065</b>	<b>16.2</b>
1.625		37.1	53.2	287	1121	44.9	16	30.45	21.0105	16.1
2.5		35.3	49.4	297	1254	51.4	19.4	35.4	24.426	14.1

- Increasing the beam pipe radius has a considerable effect on both the bandwidth and Q factor